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Figure 14: Current peak wet weather outflow from Lake Hayes #2 PS



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Figure 16: Peak wet weather outflow from Lake Hayes #2 PS using 2028 Growth Model, and including Waterfall Park Development



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Figure 17: Current peak wet weather outflow from Bendemeer PS

Document Set ID: 7544912 Version: 1, Version Date: 07/03/2023

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Figure 18: Peak wet weather outflow from Bendemeer PS using 2028 Growth Model (No Waterfall Park Development)



Beca

57:00:00 20:30:00 20:00:00 Figure 19: Peak wet weather outflow from Bendemeer PS using 2028 Growth Model, and Including Waterfall Park Development 19:30:00 00:00:67 18:30:00 00:00:8T 00:0E:71 00:00:27 J0:02:91 00:00:9T 00:0E:ST 00:00:ST 14:30:00 14:00:00 13:30:00 J3:00:00 12:30:00 12:00:00 00:02:77 00:00:TT Flow (L/s) 10:30:00 00:00:0T 00:05:6 00:00:6 8:30:00 00:00:8 7:30:00 00:00:7 00:02:9 00:00:9 5:30:00 00:00:2 4:30:00 00:00:4 3:30:00 3:00:00 2:30:00 2:00:00 J:30:00 J:00:00 0:30:00 00:00:0 140 120 100 180 160 0 60 40 20 80 s/٦

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Time

Appendix D Long Sections





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Document Set ID: 7544912 Version: 1, Version Date: 07/03/2023

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APPENDIX B

Wastewater Modelling Report Addendum





WATERFALL PARK DEVELOPMENT: WASTEWATER NETWORK ASSESSMENT

To: Distribution:	Richard Powell Jayne Richards	Queenstown Lakes District Council (QLDC) Fluent Solutions (FS)
From:	Brian Robinson; Rebec	cca Ellmers (HAL)
Subject:	Waterfall Park Develop	oment – Wastewater Network Assessment
Date:	16 January 2019	

1 Introduction

1.1 Objective

The objective of this study is to utilise the existing hydraulic model (Wakatipu Wastewater Model with HAL updates, 2018) of the Queenstown, Arrowtown and Lake Hayes wastewater network to assess the impact of the proposed Waterfall Park development on the wastewater network.

1.2 Background

The Waterfall Park development proposal seeks to discharge a maximum flow rate of 23.4 l/s to the existing network. The initial hydraulic modelling carried out by BECA (Waterfall Park Development Wastewater Modelling, 2018) considered a number of private pump station scenarios at various connection points to the existing network. The development consultant has since requested further assessment of the Waterfall Park development impact.

2 Waterfall Park Development

2.1 Overview

The Waterfall Park development seeks to discharge a maximum PWWF of 23.4 I/s and has considered two potential network connection points as summarized below:

- 1. Connection to the existing local 150mm network to the south discharging to Lake Hayes #1 Pump Station, and eventually to the Arrowtown-Lake Hayes Pump Station
- 2. Connection to the existing transmission 300mm gravity/pressure main connecting Norfolk Street Pump Station to the Arrowtown-Lake Hayes Pump Station

The connection point to the existing 150mm network to the south was shown in the assessment undertaken by Beca to result in overflows from the local network upstream of the Lake Hayes #1 pump station. This assessment has focused on the connection point to the existing 300mm gravity/pressure main with a proposed pump rate of 23.4 I/s (i.e. matching expected design flows for the full development.

The location of the development and proposed connection points is shown in Figure 1 below.







Figure 1: Waterfall Park Development Wastewater Connection

3 Waterfall Park Development Impact

3.1 Proposed Modelling Scenarios

The development consultant Fluent Solutions have since requested further assessment of the Waterfall Park development impact. The initial hydraulic modelling carried out by BECA (Waterfall Park Development Wastewater Modelling, 2018) considered a private pump station with storage and off-peak pumping (assumed to lessen the effect of the development load on the network), with an arbitrary pumped rate of 15 I/s. Fluent Solutions have requested modelling of the maximum proposed development discharge of 23.4 I/s at the Arrowtown-Lake Hayes 300mm connection point (identified as Scenario 3 in the BECA report).

3.2 Scenario 3: Waterfall Park (23.4 l/s) to Arrowtown-Lake Hayes 300mm line

The Wakatipu wastewater model (with 2018 HAL updates included update of pump station capacities) was run under the current (2015) scenario, with and without the proposed Waterfall Park development. The network was assessed against a 5-year ARI design storm to understand the system performance. As shown in the Figure 2 long-section below, the existing network has sufficient capacity in the 300mm Arrowtown-Lake Hayes Wastewater line, discharging to the Arrowtown-Lake Hayes Pump Station.







Figure 2: Existing (2015) Long Section (300mm Arrowtown WW line) – 5 year ARI design storm

The additional peak wet weather flows of 23.4 I/s from the Waterfall Park development were added in to the model, with connection to the 300mm Arrowtown-Lake Hayes wastewater line. As shown in the Figure 3 long-section below, the post-development network has adequate capacity within the 300mm line to receive the full peak wet weather flows from the proposed development.



Figure 3: Post Development (2015) Long Section (300mm Arrowtown WW line) with additional Waterfall Park Flows (23.4 I/s) – 5 year ARI design storm

It should be noted that limited information has been made available to date regarding the levels of this 300mm wastewater pipe, with modelled levels taken from QLDC's GIS which just provides invert and ground levels at the upstream end of the pipe (at the confluence with the Norfolk St and Millbrook rising mains) and at the downstream end (at the Arrowtown-Lake Hayes pump station), with no information provided regarding levels at intermediate points along its length. It is understood that this pipeline, whilst generally operating as a gravity pipe, is designed to operate under pressure if flows exceed the on-grade capacity of the pipeline





3.3 Pump Station Assessment – Current Scenario (2015)

The 300mm Arrowtown-Lake Hayes wastewater line conveys flow from the Norfolk Road Pump Station (maximum capacity 70 l/s) and the Millbrook pump station (maximum capacity 24 l/s) to the Arrowtown-Lake Hayes Pump Station. The modelled inflows and outflows for the Arrowtown-Lake Hayes PS post-development scenario are shown in Figure 4 below.

The Arrowtown-Lake Hayes Pump Station has a maximum capacity of 85 I/s with one pump operating (based on QLDC records). In the post-development scenario (with the 23.4 I/s from Waterfall Park connected), the peak modelled inflow to the pump station is 81 I/s in the 5-year ARI design storm (as shown by the red trace). As shown by the yellow trace, the majority of flows entering the pump station are received from the 300mm line and the Waterfall Park development.



Figure 4: Modelled Arrowtown-Lake Hayes Pump Station flows – 5 year ARI design storm

3.4 Pump Station Assessment – Future Scenario (2055)

Based on a future (2055) population scenario, an assessment was made of the capacities of the relevant pump stations discharging to the Arrowtown-Lake Hayes Pump Station, and can be summarised in the Figure 5 schematic below.

While there is current (2015) capacity in the Arrowtown-Lake Hayes Pump Station for the proposed development, future significant growth in the remainder of the contributing catchment (in addition to the proposed Waterfall Park flow of 23.4 l/s) will likely trigger pump station upgrade requirements.







Figure 5: Pump station capacity current (2015) scenario versus theoretical maximum flows

3.5 Pressure at Arrowtown-Lake Hayes 300mm line connection point

In both the current (2015) and future (2055) scenarios, there is sufficient capacity within the 300mm line to receive the additional flows from the Waterfall Park development. Based on the GIS data available, the wastewater line appears to discharges as free flow via gravity (i.e. not pressurized) to the Arrowtown-Lake Hayes Pump Station.

The proposed connection point of the Waterfall Park development to the Arrowtown-Lake Hayes 300mm line has been constructed in the model with an estimated ground and invert level based on existing data. Insufficient level data is available to determine whether there are sections of this pipeline that don't operate under gravity conditions (and hence may operate under pressure), and is recommended as part of the design process for the Waterfall Park development, an assessment is made of actual levels at the proposed connection point to determine whether the pipeline is expected to operate under pressure, and to determine the head that the proposed Waterfall pump station will operate at.



APPENDIX C

Water Modelling Report



Queenstown Lakes District Council Private Bag 50072 Queenstown 9348, New Zealand

Waterfall Park Development – Water Impact Assessment

19 March 2018

Mason Bros. Building Level 2, 139 Pakenham Street West Wynyard Quarter Auckland 1010 PO Box 37525, Parnell, 1151 New Zealand

T +64 (0)9 375 2400 mottmac.com This letter summarises the results of the assessment undertaken for a proposed development consisting of mixed land use, including a hotel (380 rooms) and a residential development of 125 units (double dwelling). The project is located on the northwest side of Arrowtown-Lake Hayes Rd and Speargrass Flat Rd.

1 Background

In January 2018 Mott MacDonald was commissioned by Queenstown Lakes District Council (QLDC) to assess the system performance in terms of Level of Service (LOS) and firefighting capacity in the proposed development.

In this analysis, the latest Lake Hayes water supply model was used. Three scenarios were investigated, with and without additional demand from the proposed development for existing and future conditions. These are further detailed in the scenarios investigation section of this letter.



Figure 1 - Proposed Development Location

Mott MacDonald New Zealand Limited Registered in New Zealand no. 3338812

2 Assumptions

2.1 Demand Calculations

A demand assessment was provided by the client as summarised in Table 1 below. The detailed calculation is attached in appendix.

Table 1 - Demand Calculation

Hotel Facility (Elevation: RL 368m)	
No. Hotel rooms	380
Maximum people per room	2
Peak daily consumption (I/day/room)	440
Peak water demand (m ³ /day) - room	167.2
Additional demand (conference centre, restaurant, irrigation, etc) (m ³ /day)	205.2
Instantaneous Peak Flow (I/s)	18.9

Residential Development (Elevation: RL 367m)

· · · · ·	
No. Primary Dwelling (3 people)	125
No. Secondary Dwelling (2 people)	125
Peak consumption Primary Dwelling (I/day/property)	2,100
Peak consumption Secondary Dwelling (I/day/property)	700
Peak water demand (m ³ /day)	350
Instantaneous Peak Flow (I/s)	26.7

The calculated demand seems conservative when compared to the observed consumption in Queenstown (2000l/property/day) and Lake Hayes (see table below).

Table 2 - Lake Hayes Demands

DMA Zone	Total demand (m ³ /day)	Number of connections	Average demand per connection (I/prop/day)
Shotover Country	374	495	756
Lake Hayes Estate	822	596	1379
Lake Hayes	928	421	2204
Bendeemer	17	13	1308
Terraces	25	9	2778
DMAs Combined	2,166	1,534	1,412

As shown in the table above, the proposed development peak day demand is equivalent to a third of the current peak day demand in the entire service area.

2.2 Proposed Connection Point

The minimum and maximum elevations within the proposed development areas of the lots are shown in the table below:

Table 3 - Proposed Development Elevations

	Min elevation in proposed development area	Max elevation in proposed development area
Hotel Development	347.5m (with 4 story hotel building ~12.8m height)	368m (with single story building only)
Residential Development	342m	367m

Overall, the maximum elevation within the lot proposed for the residential development is 423m.

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As suggested by the developer, it was assumed that the proposed development would be connected to the 235 mm ID main at the Arrowtown-Lake Hayes Rd and Speargrass Flat Rd junction. Figure 2 below shows the development location, and the proposed network and connection point considered in this study.



Figure 2 – Proposed Development Location, Network and Connection Point

3 Scenario Investigated

Three scenarios were investigated, including the above demand and the current network operations:

- Existing peak day scenario.
- 2028 peak day scenario.
- 2058 peak day scenario.

Planned upgrades along Frankton Ladies Mile Highway were included in the future 2028 and 2058 scenarios.

To ensure head losses in the proposed network remain between 1 and 3 m/km (recommended head losses for pipeline design), it was assumed that the proposed development would be serviced through a 260mm (ID) pipe connected to the supply point. The proposed network layout was provided by the client and is attached in appendix.

Two elevation points were included, one for the hotel (max. elevation:368m) and one for the residential development (max. elevation:367m). Respective demands were assigned to each point.

Fire flow capacity was assessed based on FW2 requirement plus sprinklers flow of 16.6l/s, as defined by the client.

4 Model Results

4.1 System Performance Analysis in the Proposed Development

This section describes the results of the system performance analysis undertaken for the above scenarios after including the proposed development demands. Results have been analysed to verify whether levels of service can be met in the proposed development without any network modification. The table below summarises the results in terms of minimum and maximum pressure, maximum head losses in the proposed network (260mm pipe) and fire flow capacity.

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Table 4 - Minimum Pressure and Maximum Head Losses in Proposed Development

Scenario	Minimum Pressure (m)	Maximum Pressure (m)	Maximum Head Losses (m/km)	Fire Flow
Existing	60.9	97.1	3.0	Can meet residential
2028	59.9	97.1		fire flow (FW2 –25 l/s + 16 6l/s sprinklers
2058	58.0	97.0		flow)

The normal operating pressure set by QLDC addendum to NZS4404:2004 (Development ad Subdivision Engineering Standards) is 30 to 90m. As shown in the table above, minimum pressure in the proposed development is predicted to meet the recommended LOS for all scenarios. However, pressures higher than the recommended LOS are predicted in areas below 349m.

FW2 fire flow was tested at the end of the proposed 260mm (ID) line. The model predicts that residential fireflow (FW2 – 25I/s) plus the sprinkler flow required can be provided with a residual pressure of 47m at RL 368m.

The highest elevation that would be serviceable for the residential development is 395m. Recommended LOS in terms of pressure and fire flow are predicted to be met up to this point.

4.2 System Performance Analysis in the Remaining of the Network

The section below describes the results of the system performance in the remaining of the Lake Hayes network. Results have been analysed to assess the effect of the proposed development for each scenario.

Figure 3 to Figure 8 below show the system performance for current operational conditions, including current, 2028 and 2058 peak demand.

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Figure 3 – Current Peak Day System Performance – Prior Development



Figure 4 – Current Peak Day System Performance - Post Development

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Figure 5 - 2028 Peak Day System Performance - Prior Development



Figure 6 - 2028 Peak Day System Performance - Post Development

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Figure 7 - 2058 Peak Day System Performance - Prior Development



Figure 8 - 2058 Peak Day System Performance - Post Development

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The table below summarises the maximum head losses in the existing 235mm ID pipe along Arrowtown Lake Hayes Rd and the minimum pressure forecasted at the supply point, before and after the proposed development:

Table 5 - Minimum Pressure at Supply Point

Demand	Min pressure before development (m)	Min pressure after development (m)	Pressure drop (m)
Current Peak Day	89.5	83.1	6.4
2028 Peak Day	89.2	82.2	7.0
2058 Peak Day	88.2	80.2	8.0

Table 6 - Maximum Head Losses in 235mm ID Pipe

Demand	Max head losses before development (m/km)	Max head losses after development (m/km)	Head losses increase (m/km)
Current Peak Day	0.4	6.0	5.6
2028 Peak Day	0.6	6.6	6.0
2058 Peak Day	1.1	7.8	6.7

As shown in the pictures and above tables, the proposed development is predicted to have a noticeable impact on the remaining of the water network with a maximum pressure drop of 8.0m. Pressures are generally high along Arrowtown Lake Hayes Rd and Speargrass Flat Rd, so pressure remains well above the recommended LOS in this area, for current and future scenarios. However, pressures below the recommended LOS are predicted in the properties located in the elevated areas of Slope Hill Rd and Threewood Rd. This is an existing LOS issue that needs to be addressed.

Head losses are predicted to increase by up to 6.7m/km reaching 7.8m/km in the 235mm (ID) along Arrowtown Lake Hayes Rd due to the additional demand. The predicted head losses exceed the recommended LOS, 5m/km. This LOS issue needs to be addressed.

5 Conclusions and Recommendations

Demand from the proposed Waterfall Park development has been added to the network for the current, future 2028 and 2058 peak day models to determine if suitable levels of service could be obtained.

Levels of service are expected to be met in terms of minimum pressure and head losses in the proposed development, however pressures higher than the recommended LOS are predicted in areas below 349m. The model predicts that fireflow requirements (FW2 – 25l/s and 16.6l/s sprinklers flow) can be provided with a residual pressure of 47m at RL 368m, for current and future scenarios. The highest elevation that would be serviceable for the residential development is 395m.

The system performance in the remaining of the network has been verified. The proposed development is predicted to cause a maximum pressure drop of 8m at the connection point. Since pressures are high in this area recommended LOS can still be met in terms of pressure. However, pressures dropping to zero are predicted in 2058 in properties located in the elevated areas of Slope Hill Rd and Threewood Rd due to the additional demand. These areas already experience pressures below the recommended LOS, the additional demand causes the pressure to deteriorate even further.

Maximum head losses greater than 5 m/km are predicted along Arrowtown Lake Hayes Rd for all scenarios. This system performance issue is related to the additional demand, the proposed development impact needs to be mitigated.

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Diana Galindo Hydraulic Engineer diana.galindo@mottmac.com

Revision	Date	Originator	Checker	Approver	Description
A	23/02/2018	Diana Galindo	Julie Plessis	Julie Plessis	Draft for client review
В	19/03/2018	Diana Galindo	Julie Plessis	Julie Plessis	Draft for client review
С	30/05/2018	Diana Galindo	Nasrine Tomasi	Nasrine Tomasi	Final

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6 Appendix - Demand Calculation and proposed Pipe Layout

Waterfall Park Water Demand Estimate Summary										
Table 1: Waterfall Park Hotel Comple	Fable 1: Waterfall Park Hotel Complex - Water Demand Estimate									
			Average Daily	Average Daily						
		Max no.	Water	Water	Average Daily	Peak Hour	Peak Hour	Peak Day		
	No.	People /	Demand	Demand	Water	Peaking	Demand	Peaking	Peak Day	
Hotel facility	Facilities	Facility	(L/p/d)	(m3/day)	Demand (L/s)	Factor	(L/s)	Factor	Demand (L/s)	Comment / Reference
Hotel Room	380	2	220	167.2	1.94	6.6	12.77	3.30	6.39	AS/NZS 1547:2012, Table H4.
Conference Centre	1	600	30	18	0.21	6.6	1.38	3.30	0.69	Metcalfe and Eddy, Table 3-2. Wedding can occur at same time as conference
										AS/NZS 1547:2012, Table H4. Restaurants can seat 270 people. Assume hotel full
										(760 people) asssume each person eats two meals at hotel, total no. diners = 1520
Restaurants	1	1520	30	45.6	0.53	6.6	3.48	3.30	1.74	over a day
										AS/NZS 1547:2012, Table H4. Lounge and bar can accommodate 115 people, assume
Lounge Bar and bar	1	250	20	5	0.06	6.6	0.38	3.30	0.19	250 people max over a day
Chapel / wedding venue	1	100	40	4	0.05	6.6	0.31	3.30	0.15	Assume 40L/guest. Wedding can occur at same time as conference.
										Metcalfe and Eddy Table 3-4 for swimming pools. Assume pool is filled overnight
Wellness centre - pool, gym, spa	1	100	40	4	0.05	б.б	0.31	3.30	0.15	when irrigation is not running.
Non residential staff	1	120	30	3.6	0.04	б.б	0.28	3.30	0.14	AS/NZS 1547:2012, Table H4.
										Based on calculated irrigation requirements with irrigation over an eight hour period
Irrigation demand	1	n/a	n/a	125	1.45	n/a	n/a	n/a	4.35	overnight
Total				372.59	4.31		18.90		13.80	

able 2: Waterfall Park Residential Development - Water Demand Estimate										
			Average Daily	Average Daily						
		No.	Water	Water	Average Daily	Peak Hour	Peak Hour	Peak Day		
	No.	people/	Demand	Demand	Water	Peaking	Demand	Peaking	Peak Day	
Hotel facility	Dwellings	dwelling	(L/p/d)	(m3/day)	Demand (L/s)	Factor	(L/s)	Factor	Demand (L/s)	Comment / Reference
Primary Dwelling	125	3	700	262.5	3.04	6.6	20.05	3.30	10.03	Total of 125 lots
										Assume each lot may also have a secondary dwelling. Assume average of 2 person
										occupancy per secondary dwelling, assume no irrigation requirements for secondary
Secondary Dwelling	125	2	350	87.5	1.01	6.6	6.68	3.30	3.34	dwelling
Total				350.00	4.05		26.74		13.37	

Notes:

- Average day to peak hour peaking factor of 6.6 has been applied as per QLDC CoP Section 6.3.5.6

- The average day to peak day peaking factor is assumed to be 50% of average day to peak hour peaking factor

- It is assumed that each residential lot may have a primary dwelling and a secondary dwelling

References:

Metcalfe and Eddy, 2003, Wastewater Engineering: Treatment and Reuse, McGraw-Hill AS/NZS 1547:2012 - Onsite wastewater management QLDC Land Development and Subdivision Code of Practice, 2015

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APPENDIX D

Email Correspondence on Fire Fighting Requirements

Louise Clarke

From:	Sam Ballam <sam.ballam@ppgroup.co.nz></sam.ballam@ppgroup.co.nz>
Sent:	Thursday, 24 June 2021 1:59 pm
То:	Louise Clarke; Lauren Christie; Jayne Richards
Cc:	Tim Allan; damien@oceaniafireprotection.co.nz; David Chenery
Subject:	RE: [PPG-Q6388D] Ayrburn - Fire Engineering and Water Demands

Hi Louise,

Below is previous correspondence I found from David, noting the this is for the heritage buildings and doesn't account for the future homestead and hay barn buildings.

"I just spoke with Cam Stewart at GHD. They have done the sprinkler design for Oceania. Flow rate required is 800 l/min at 300 Kpa"

Jayne – Can you confirm your understanding, I haven't been back through all the correspondence but from memory the haybarn had the biggest fire cell demand and you were going to take an estimate at what the peak demand would be.

Regards,

Sam Ballam

Licensed Cadastral Surveyor, MS+SNZ Queenstown Office M 027 427 4557 E sam.ballam@ppgroup.co.nz

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From: Louise Clarke <louise@fluentsolutions.co.nz>
Sent: Thursday, 24 June 2021 11:47 am
To: Sam Ballam <sam.ballam@ppgroup.co.nz>; Lauren Christie <Lauren.Christie@winton.nz>
Cc: Tim Allan <t.allan@brynmartin.co.nz>; damien@oceaniafireprotection.co.nz
Subject: RE: [PPG-Q6388D] Ayrburn - Fire Engineering and Water Demands

Hi Sam,

Had the sprinkler demand been confirmed? I know the backflow prevention was resolved, but I cant identify a confirmation on the flows for sprinklers.

Regards, Louise



APPENDIX E

Hydraulic Calculations

Hydraulic calcs comparing to model

Hydraulic Calculations to assess maximum headlosses in 235mm ID pipe Q000492 Ayrburn Domain Louise Clarke Jayne Richards

Title Job No. Job Title:

Engineer:

Checked:

	Date:	1/11/2021												
re-development flows - estimated from Mott MacDonald Headloss/km in Table 6 (to match headloss in m/km)														
Pipe Dia (ID)	Flow	Area	Pipe diameter	Roughness Coefficient	Length	Kinematic Viscosity	Mean Velocity	Hydraulic diameter	Reynolds Number	Friction Coefficient	Total Head loss		Velocity Head	Description
	Q (l/s)	A (m ⁻)	m	k (mm)	L (m)	v (10 ^{-o} m²/s)	V (m/s)	D (m)	Re	f	∆H (m)	m/1000 m		
235 mm	12.7	0.04338	0.235	0.015	1	1.5	0.29	0.235	45867	0.0214	0.00	0.40	0.004368623	Estimated flow before development- current peak day
235 mm	16	0.04338	0.235	0.015	1	1.5	0.37	0.235	57785	0.0204	0.00	0.60	0.006933893	Estimated flow before development- 2028 peak day
235 mm	22.4	0.04338	0.235	0.015	1	1.5	0.52	0.235	80899	0.0190	0.00	1.10	0.01359043	Estimated flow before development- 2058 peak day

Post-development flows - estimated from Mott MacDonald Headloss/km in Table 6 (to match headloss in m/km)														
Pipe Dia (ID)	Flow	Area	Pipe diameter	Roughness Coefficient	Length	Kinematic Viscosity	Mean Velocity	Hydraulic diameter	Reynolds Number	Friction Coefficient	Total Head loss		Velocity Head	Description
	Q (l/s)	A (m ⁻)	m	k (mm)	L (m)	v (10 ^{°°} m ² /s)	V (m/s)	D (m)	Re	f	∆H (m)	m/1000 m		
235 mm	57	0.04338	0.235	0.015	1	1.5	1.31	0.235	205859	0.0160	0.01	6.00	0.088000853	Estimated flow post development- current peak day
235 mm	60	0.04338	0.235	0.015	1	1.5	1.38	0.235	216694	0.0159	0.01	6.59	0.09750787	Estimated flow post development- 2028 peak day
235 mm	65.8	0.04338	0.235	0.015	1	1.5	1.52	0.235	237641	0.0156	0.01	7.81	0.117270548	Estimated flow post development- 2058 peak day

Current peak day:	44.3 L/s				
2028 peak day:	44 L/s				
2058 peak day:	43.4 L/s				
New flow (Waterfall Park Hotel plu	s Northbrook Retirement Village):				
New flow (Waterfall Park Hotel plus	s Northbrook Retirement Village):				
New flow (Waterfall Park Hotel plu: Current peak day:	s Northbrook Retirement Village): 29.8 L/s				
New flow (Waterfall Park Hotel plu: Current peak day: 2028 peak day:	s Northbrook Retirement Village): 29.8 L/s 29.8 L/s				

New post-development flows (Mott Macdonald Pre-Development Flows plus Waterfall Park Hotel plus Northbrook Retirement Village):							
Current peak day:	42.5 L/s						
2028 peak day:	45.8 L/s						
2058 peak day:	52.2 L/s						

vew post-development flows (Mott Macdonald Pre-Development Flows plus Waterfall Park Hotel plus Northbrook Retirement Village):														
Pipe Dia (ID)	Flow	Area	Pipe diameter	Roughness Coefficient	Length	Kinematic Viscosity	Mean Velocity	Hydraulic diameter	Reynolds Number	Friction Coefficient	Total Head loss		Velocity Head	Description
	Q (I/s)	A (m ²)	m	k (mm)	L (m)	v (10 ^{-o} m ² /s)	V (m/s)	D (m)	Re	f	∆H (m)	m/1000 m		
235 mm	42.5	0.04338	0.235	0.015	1	1.5	0.98	0.235	153491	0.0169	0.00	3.51	0.04892322	Estimated flow post development- current peak day
235 mm	45.8	0.04338	0.235	0.015	1	1.5	1.06	0.235	165409	0.0166	0.00	4.02	0.056815669	Estimated flow post development- 2028 peak day
235 mm	52.2	0.04338	0.235	0.015	1	15	1 20	0 235	188523	0.0163	0.01	5 11	0 073803707	Estimated flow post development- 2058 peak day

Extract from Mott Macdonald Report:

The table below summarises the maximum head losses in the existing 235mm ID pipe along Arrowtown Lake Hayes Rd and the minimum pressure forecasted at the supply point, before and after the proposed development:

Table 5 - Minimum Pressure at Supply Point

Demand	Min pressure before development (m)	Min pressure after development (m)	Pressure drop (m)
Current Peak Day	89.5	83.1	6.4
2028 Peak Day	89.2	82.2	7.0
2058 Peak Day	88.2	80.2	8.0

Table 6 - Maximum Head Losses in 235mm ID Pipe

Demand	Max head losses before development (m/km)	Max head losses after development (m/km)	Head losses increase (m/km)
Current Peak Day	0.4	6.0	5.6
2028 Peak Day	0.6	6.6	6.0
2058 Peak Day	1.1	7.8	6.7

As shown in the pictures and above tables, the proposed development is predicted to have a noticeable impact on the remaining of the water network with a maximum pressure drop of 8.0m. Pressures are generally high along Arrowtown Lake Hayes Rd and Speargrass Flat Rd, so pressure remains well above the recommended LOS in this area, for current and future scenarios. However, pressures below the recommended LOS are predicted in the properties located in the elevated areas of Slope Hill Rd and Threewood Rd. This is an existing LOS issue that needs to be addressed.

Head losses are predicted to increase by up to 6.7m/km reaching 7.8m/km in the 235mm (ID) along Arrowtown Lake Hayes Rd due to the additional demand. The predicted head losses exceed the recommended LOS, 5m/km. This LOS issue needs to be addressed.

WATERFALL PARK DEVELOPMENTS LTD **NORTHBROOK - ARROWTOWN RESOURCE CONSENT DRAWINGS**

PLAN INDEX

SHEET	CONTENTS	REV	DATE
INDEX			
001	INDEX SHEET	С	28/02/2023
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100	SITE PLAN	C	28/02/2023
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EARTHWO	RKS		
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400	STORMWATER OVERVIEW	С	28/02/2023
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410	WETLAND SECTIONS	С	28/02/2023
\\/\ASTF\\/A	TER/WATER		
500	WASTEWATER/WATER OVERVIEW	C	28/02/2023
501-503	WASTEWATER/WATER DETAIL	C	28/02/2023
201 202		C	20,02,2020

BY: Sb

FOR	RESOURCE CONSENT						
REV.	REVISION DETAILS	DATE					
А	DRAFT ISSUE	30/03/22					
В	FOR RESOURCE CONSENT	27/09/22					
С	RFI RESPONSE	28/02/23					
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E queenstown@ppgroup.co.nz

ation:	
WATERFALL P	ARK
DEVELOPMENT	S LTD
LOT 1 DP 5407	788

Purpose/Drawing Title

NORTHBROOK - ARROWTOWN **INDEX SHEET**

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JRN DOMAIN)		LEGAL BOUNE LEGAL BOUNE UNDERLYING MILL CREEK SITE EXTENTS PROPOSED BI AYRBURN BU GRASS SWALI CONCRETE CI CUT / FILL INT EARTH BATTE RETAINING W ROAD CARRIA CYCLE / PEDE CONCRETE TI STONE THRES	DARY (SUI DARY (ABI BOUNDAI S UILDING ILDINGS (E HANNEL / ERFACE R EXTEN ALL AGEWAY ESTRIAN F HRESHOL SHOLD	BJECT PROPERTY) JTTALS) RY (ROAD TO BE R UNDER CONSTRUC KERB T PATH D / PARKING AREA	EALIGNED)		
5	POND / RAINGARDEN - 366.0 — PROPOSED CONTOUR (1m INTERVAL) REV. REVISION DETAILS DATE A ORIGINAL ISSUE 30/03/22 B FOR RESOURCE CONSENT 27/09/22 C RFI RESPONSE 28/02/23 C RFI RESPONSE 28/02/23 D D D D D D D D D D D D D D D D D D D						
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BY: Sb



MILL CREEK

SITE EXTENTS

PROPOSED ROAD

PROPOSED PATH

CONSENTED HOTEL BUILDING (RM180584)

PROPOSED BUILDING

AYRBURN BUILDINGS (UNDER CONSTRUCTION)

CONSENTED ROAD / PATH (RM180584)

EXISTING ROAD / PATH

NOTES

1. EXISTING WATERFALL PARK ROAD BOUNDARY TO BE EXISTING WATERFALL PARK ROAD BOUNDARY TO BE REALIGNED TO SUIT PROPOSED ROAD ALIGNMENT. PROPOSED LEGAL BOUNDARIES SHOWN RELATE TO AN EXISTING ROAD STOPPING APPLICATION LODGED WITH QLDQ WHICH IS STILL SUBJECT TO APPROVAL.



FOR RESOURCE CONSENT

REV.	REVISION DETAILS	DATE
А	ORIGINAL ISSUE	30/03/22
В	FOR RESOURCE CONSENT	27/09/22
С	RFI REPSONSE	28/02/23

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WATERFALL PARK DEVELOPMENTS LTD LOT 1 DP 540788

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NORTHBROOK - ARROWTOWN RM180584 CONSENT OVERLAY

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LEGEND

	LEGAL BOUNDARY (SUBJECT PROPERTY)
	LEGAL BOUNDARY (ABUTTALS)
<u> </u>	UNDERLYING TITLE BOUNDARY (ROAD TO BE REALIGNED)
	MILL CREEK
0.50 —	CUT AREA / CONTOUR (0.5m INTERVAL)
0.50	FILL AREA / CONTOUR (0.5m INTERVAL)
-0.00	ZERO CUT / FILL CONTOUR
357.0	DESIGN CONTOURS (1m INTERVAL)
-357-0	EXISTING CONTOURS (1m INTERVAL)
	RETAINING WALL
	EXTENT RM180584 WORKS UNDER CONSTRUCTION
1	SITE EXTENTS

<u>NOTES</u>

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- SEE ROADING SHEETS (300 306) FURTHER DETAIL OF PROPOSED CONTOURS. REFER SHEETS 211-212 FOR FURTHER DETAIL OF DEPTH 2.
- CONTOURS FOR CLARITY DEPTH CONTOURS HAVE BEEN SHOWN TO GROUND LEVEL, ADDITIONAL DEPTH WILL BE REQUIRED FOR EXCAVATION OF BASEMENT 3.
- EXCAVATION OF BASEMENT EARTHWORKS QUANTITIES SHOWN ARE REPRESENTATIVE OF DESIGN DEVELOPED TO CONSENT LEVEL DETAIL. QUANTITIES WILL BE SUBJECT TO FLUCUATION AS DESIGN IS DETAILED FOLLOWING CONSENT, VOLUMES WILL BE REPRESENTATIVE OF THE LANDFORM AT THE TIME.

EARTHWORKS

5.

- TOPSOIL 5.1 STRIP 5.2 RESPREAD
- 5.3 EXCESS
- 5.3 EXCESS EARTHWORKS 6.1 CUT FILL 6.2 CUT WASTE IMPORTED MATERIAL
- IMPORTED MATERIAL

 T.1 ENGINEERED FILL SPEC
 Z ROADING / PATH AGGREGATES

 MAX CUT DEPTH, MAX FILL DEPTH
 AREA OF EARTHWORKS

10,000m³ 5,000m³ 5,000m³ 5,000m³ 7,000m³

25,000m³ 4,000m³ 6.0m 6.5 Ha

FOR RESOURCE CONSENT

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LEGEND

	LEGAL BOUNDARY (SUBJECT PROPERTY)
	LEGAL BOUNDARY (ABUTTALS)
<u> </u>	UNDERLYING TITLE BOUNDARY (ROAD TO BE REALIGNED)
	MILL CREEK
— 0.50 —	CUT AREA / CONTOUR (0.5m INTERVAL)
—- 0 .50 —	FILL AREA / CONTOUR (0.5m INTERVAL)
	ZERO CUT / FILL CONTOUR
<u> </u>	DESIGN CONTOURS (1m INTERVAL)
	EXISTING CONTOURS (1m INTERVAL)
	RETAINING WALL
	EXTENT RM180584 WORKS UNDER CONSTRUCTION
L=1	SITE EXTENTS

<u>NOTES</u>

- SEE ROADING SHEETS (300 306) FURTHER DETAIL OF 1.
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- 3.
- REFER SHEETS 211-212 FOR FURTHER DETAIL OF DEPTH CONTOURS FOR CLARITY DEPTH CONTOURS HAVE BEEN SHOWN TO GROUND LEVEL, ADDITIONAL DEPTH WILL BE REQUIRED FOR EXCAVATION OF BASEMENT EARTHWORKS QUANTITIES SHOWN ARE REPRESENTATIVE OF DESIGN DEVELOPED TO CONSENT LEVEL DETAIL. QUANTITIES WILL BE SUBJECT TO FLUCUATION AS DESIGN IS DETAILED FOLLOWING CONFENT, YOU WARD WILL DE DEPERSENTATIVE 4. FOLLOWING CONSENT, VOLUMES WILL BE REPRESENTATIVE OF THE LANDFORM AT THE TIME.

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Version: 1, Version Date: 07/03/2023

LEGEND

	LEGAL BOUNDARY (SUBJECT PROPERTY)
	LEGAL BOUNDARY (ABUTTALS)
<u> </u>	UNDERLYING TITLE BOUNDARY (ROAD TO BE REALIGNED
	MILL CREEK
— 0.50 —	CUT AREA / CONTOUR (0.5m INTERVAL)
—- 0 .50 —	FILL AREA / CONTOUR (0.5m INTERVAL)
-0.00	ZERO CUT / FILL CONTOUR
	DESIGN CONTOURS (1m INTERVAL)
	EXISTING CONTOURS (1m INTERVAL)
	RETAINING WALL
	EXTENT RM180584 WORKS UNDER CONSTRUCTION
L1	SITE EXTENTS

<u>NOTES</u>

- SEE ROADING SHEETS (300 306) FURTHER DETAIL OF PROPOSED CONTOURS.
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FOR RESOURCE CONSENT

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LEGEND

	LEGAL BOUNDARY (SUBJECT PROPERTY)
	LEGAL BOUNDARY (ABUTTALS)
<u> </u>	UNDERLYING TITLE BOUNDARY (ROAD TO BE REALIGNED)
	MILL CREEK
— 0.50 —	CUT AREA / CONTOUR (0.5m INTERVAL)
—-0.50 —	FILL AREA / CONTOUR (0.5m INTERVAL)
-0.00	ZERO CUT / FILL CONTOUR
357.0	DESIGN CONTOURS (1m INTERVAL)
	EXISTING CONTOURS (1m INTERVAL)
	RETAINING WALL
	EXTENT RM180584 WORKS UNDER CONSTRUCTION
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<u>NOTES</u>

- 1.
- SEE ROADING SHEETS (300 306) FURTHER DETAIL OF PROPOSED CONTOURS. REFER SHEETS 211-212 FOR FURTHER DETAIL OF DEPTH CONTOURS 2.
- 3.
- CONTOURS FOR CLARITY DEPTH CONTOURS HAVE BEEN SHOWN TO GROUND LEVEL, ADDITIONAL DEPTH WILL BE REQUIRED FOR EXCAVATION OF BASEMENT EARTHWORKS QUANTITIES SHOWN ARE REPRESENTATIVE OF DESIGN DEVELOPED TO CONSENT LEVEL DETAIL QUANTITIES WILL BE SUBJECT TO FLUCUATION AS DESIGN IS DETAILED FOLLOWING CONSENT, VOLUMES WILL BE REPRESENTATIVE OF THE LANDFORM AT THE TIME Δ OF THE LANDFORM AT THE TIME.

FOR RESOURCE CONSENT

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	LEGEND	
A.		LEGAL BOUNDARY
	1-1	SITE BOUNDARY
		MILL CREEK
		UPSTREAM WORKS EXTENT (UNDER CONSTRUCTION RM180584)
		PROPOSED BUILDING
		STORMWATER CATCHMENT
	<u> </u>	DESIGN CONTOURS (1m INTERVAL)
		SEDIMENT RETENTION POND (SRP)
SITE		GRAVEL LAYDOWN / HAUL ROAD (EXISTING)
		CLEAN WATER DIVERSION CHANNEL
		DIRTY WATER DIVERSION CHANNEL
		TEE BAR DECANT
		SW PIPE
		SILT FENCE
	$\langle \neg$	OVERLAND FLOW DIRECTION

<u>NOTES</u>

- SEDIMENT AND EROSION CONTROLS TO BE ESTABLISHED 1. PRIOR TO COMMENCING WORKS.
- ALL SEDIMENT AND EROSION CONTROLS TO BE ESTABLISHED IN ACCORDANCE WITH AUCKLAND COUNCIL GD05 2.
- PERIMETER OF ALL WORK AREAS TO BE PROTECTED BY EITHER EARTH BUND OR SILT FENCE TO PREVENT DISCHARGE 3. OF ANY SEDIMENT LADEN RUNOFF TO MILL CREEK 4. THIS PLAN IS A DRAFT CONCEPT TO BE USED FOR RESOURCE
- CONSENT APPLICATION ONLY, FURTHER DETAIL TO BE ADDED PRIOR TO SUBMISSION FOR CONSTRUCTION APPROVAL OR IMPLEMENTATION. CATCHMENTS SHOWN WILL BE SUBJECT TO CHANGE AS THE DETAILED DESIGN DEVELOPS AND TO REPRESENT THE LANDFORM AT THE TIME.

FOR RESOURCE CONSENT

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NOTES

- 1. EXISTING WATERFALL PARK ROAD BOUNDAR REALIGNED TO SUIT PROPOSED ROAD ALIGH PROPOSED LEGAL BOUNDARIES SHOWN REI EXISTING ROAD STOPPING APPLICATION LO 2. NO CHANGE TO HORIZONTAL GEOMETRY OF
- NO CHANGE TO HORIZONTAL GEOMETRY OF FROM RM180584 BETWEEN CH1040 AND CH1
 ROAD WIDENING MAY BE REQUIRED TO ACC VEHICLE SWEPT PATHS, EXTENT OF WIDENII ASSESSED AT DETAILED DESIGN.
- WATERFALL PARK ROAD ALIGNMENT WILL B PREVENT EVERYDAY ACCESS. THIS SECTION
 - WILL ONLY BE ACCESSIBLE AS OPERATIONS
 PARKING FOR THE RESIDENTIAL LTO BUILDIN PROVIDED IN THE BASEMENT, REFER TO WC
 - DRAWINGS FOR DETAILS. 6. ALL RETAINING WALLS ARE MAX 1m HIGH UN
- ALL RETAINING WALLS ARE MAX 1m HIGH UNI OTHERWISE.
 RETAINING WALL HIGHS SHOWN ARE FOR INE PURPOSES ONLY, FINAL STRUCTURES WILL E DETAILED DESIGN.
 PATHS SHOWN ON THESE DRAWINGS ARE LII LINKAGES, REFER TO LANDSCAPE AND ARCH DRAWINGS FOR MORE DETAIL OF PATHS / PA DRAWINGS FOR MORE DETAIL OF PATHS / PA
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		STABILISED GRASS (EMERGENCY PARKIN	IG)
		PAVING AREA	
		WORKS COMPLETED UNDER RM180584	
	6	EXISTING TREE	
	C.	POND / RAINGARDEN	
	- 366.0	PROPOSED CONTOUR (0.5m INTERVAL)	
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Approved by:

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NORTHBROOK - ARROWTOWN **ROADING OVERVIEW**

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LEGEND



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Version: 1, Version Date: 07/03/2023





Version: 1, Version Date: 07/03/2023

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LEGEND

- PUBLIC PATH (2.5 3.0m WIDE), ACCESSIBLE
- ACCESSIBLE PATH (MAX 3%)
- ACCESSIBLE PATH (MAX 5% WITH LANDINGS
- ACCESSIBLE PATH (MAX 8% WITH LANDINGS
- NOT ACCESSIBLE (MAX 12% OR STAIRS)

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-	Purpose/Dr NOI AC	awing Title: RTHBRO CESSIBL y:	OK - A E PA	ARRO THS L	WTOV AYOU 1:2500 OT SCALI 28/02/20	







	VIP CH. 758.90 RL.347.18	VTP CH. 777.93 RL.348.74	 VIP CH. 796.97 RL:350.30 	- VTP CH. 816.00 RL.350.68						 VTP CH. 908.47 RL.352.54 	- VIP CH. 922.00 RL.352.82	 VTP CH. 935.53 RL.352.48 	 VTP CH. 952.21 RL.352.06 VIP CH. 955.71 RL.351.99 SAG CH. 955.785 RL.351.99 	VTP CH. 959.21 RL.351.99	 VTP CH. 978.96 RL.352.11 	 VIP CH. 984.46 RL.352.15 	 VTP CH. 989.96 RL.352.30
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+ FILL DEPTH).48).49).50	0.71 0.75 1.20 1.40	1.36 1.18 1.18	1.17 1.15 1.08 1.04 0.90	.81).79).64).45).45	0.22 0.29 1.89	2.32	2.13	2.28 2.28 2.07	1.17 1.17 0.29 0.86).78).67).57).50).53).51).50).51 1 42	1.03	1.03
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CHAINAGE	750.00 758.90 760.00	768.68 770.00 777.93 780.00	796.97 800.00	808.41 810.00 816.00 820.00 825.36 825.36 820.00	840.00	850.00 860.00	868.62	880.00 881.04 890.00	892.42 900.00	908.47 910.00	920.00 920.53 922.00	930.00 935.53 940.00 943.42	950.00 952.21 955.71	955.85 957.85 959.21	960.00 962.80 970.00	978.96 980.00	983.60 984.46
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BY: Sb



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HORIZ CURVE DATA

DATUM R.L.316.00 EXISTING GROUND

+ FILL DEPTH

- CUT DEPTH

DESIGN LEVEL

CHAINAGE

LEVEL

VERTICAL GRADE VERTICAL LENGTH

BY: Sb

PLOT DATE:	03 March, 2023 - 2:34 PM
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Version: 1, Ver	sion Date: 07/03/2023

										VIP CH. 10/6./9 KL.354./3		VIP CH. 1091./9 KL.355.15		 VTP CH. 1106.79 RL.355.45 									- VITD CH 1170 25 PI 356 00	- VIF CH. 11/8.20 NL.300.30	 VIP CH. 1188.62 RL.357.09 	110 00 110 HO UTV	VIPCH. 1191.98 KL.331.44	VIP CH. 1207.35 RL.357.80		 VTP CH. 1216.71 RL.357.90 				VTP CH. 1249.26 RL.358.22
Z CURVE DATA		R-100.0)0m >> <	<u></u> R-12 <u>.0</u>	0m <u>-</u>				F	50.00)m	.>			+			<	R-40.0)0m -	>	~	- R	40.0	0m							< R	-60.00	m
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STING GROUND EL	351.22	351.56	352.52 352.77 353.37 353.79	354.44	354.43 354.41	354.41	354.52	354.63 354.66	354.65	354.71	354.77	354.76 264.75	354.75	354.70 354.67	354.60	354.65	354.67	354.83	355.10	355.82	356.08	356.21	356.18	356.16	356.71 356.88	356.71	356.68	356.68 356.79	356.63	357.00 357.16	357.29	357.29	357.55	357.76
LL DEPTH IT DEPTH	1.08	1.02	0.34 0.15 -0.31 -0.65	-1.02	-0.84 -0.71	-0.43	-0.26	-0.21	0.08	0.11	0.31	0.36	0.56	0.75	0.04 1.11	1.26	1.34	1.29	1.21	0.69	0.51	0.50	0.72	0.76	0.41 0.29	0.73	0.83	0.84 0.95	1.16	0.90	0.74	0.74	0.58	0.47
GIGN LEVEL	352.30	352.58	352.86 352.92 353.06 353.14	353.42	353.59 353.70	353.98	354.26	354.42 354.54	354.73	354.82	355.08	355.12 255.70	355.31 355.31	355.45 355.45	355.71	355.91	356.01	356.11	356.31	356.51	356.59	356.71	356.90	356.92	357.13 357.17	357.44	357.51	357.52 357.74	357.79	357.90 357.93	358.03	358.03	358.13	358.22
AINAGE	00.066	1000.00	1010.00 1012.17 1017.03 1020.00	1030.00	1036.10	1050.00	1060.00	1065.55	1076.79	1080.00	1090.00	1091.79	1100.00	1106.79	1120.00	1130.00	1134.95	1140.00	1150.00	1160.00	1163.80	1170.00	1179.25	1180.00	1188.62 1190.00	1197.98	1199.83	1200.00 1207.35	1210.00	1216.71 1220.00	1229.86	1230.00	1240.00	1249.26
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SCALE: 1:500





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- DESIGN SURFACE

----- EXISTING SURFACE

FOR RESOURCE CONSENT

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REV.	REVISION DETAILS		DATE
А	ORIGINAL ISSUE		30/03/22
В	FOR RESOURCE CONS	ENT	27/09/22
С	RFI RESPONSE		28/02/23
P Su	ATERSON rveying • Planr Your Land Pro WWW.ppg 0800 1	DITTSGRO	UP ering
QUEE Terrac 1092 PO Bo Quee T 03 4 E quee	ENSTOWN: ce Junction, Frankton Road. ox 2645, nstown 9349. 141 4715 instown@ppgroup.co.nz	© COPYRIGHT. This drawing, design remains the property of Pitts LP and may not be reprov or full or altered without the wr permission of Paterson Pitts LI drawing and its content shall o for the purpose for which it is liability shall be accepted by P. LP for its unauthorised use.	content, and Paterson duced in part itten P. This nly be used ntended. No aterson Pitts
Client/Local	WATERF DEVELOPN LOT 1 DI	ALL PARK /IENTS LTI P 540788)
Purpose/Dr NOF R	aving Title: RTHBROOK OAD 01 LO	- ARROWTO	NWC N
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SB

SP

Drawn by:

Checked by:

Approved by:

Q6388 - 82 - 01

A3

Sheet No: 321

DO NOT SCALE

evision No: Date Issued: 28/02/2023

			VTP CH. 1249.26 RL.358.22			VIP CH. 1264.26 RL.358.37			VIP CH. 12/9.20 KL.359.5/						- VTP CH 1317 80 BI 362 66	 VIP CH. 1322.89 RL.363.06 	 VTP CH 1327 89 RI 363 30 							- VTP CH. 1368.78 RL.365.22	VIPCH 1378 78 RI 365 60		TTP CH. 1388.78 RL.366.73			VTP CH 1406 82 BI 368 60		VIP CH. 1416.82 RL.369.63		VTP CH. 1426.82 RL.369.69			VTP CH. 1446.78 RL.369.80	VIP CH. 1451.78 RL.369.82	VIP CH. 1456./8 KL.309.84	CREST CH. 1465.04 RL.369.88	VIP CH. 1469.17 RL.369.89	VTP CH. 1474.17 RL.369.68				VTP CH. 1516.52 RL.367.91	The CH. 1520 40 RL 367 82 VTP CH. 1521 52 RL 367 83	
	HORIZ CURVE DATA		60.0) m E	<u>250.0</u>	<u>مور</u>				<u>R5</u>)_00i	<u>т</u> .	V	_	R-60	.00rr	1 -		-		-		R35.0	00m	_	>	~	– F	२-35.	00m	_	>						Ц	₹ <u>50.</u> С	<u>)0m</u>	>				F	२- <u>३०</u> -	00m	1
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- CUT DEDLH - 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- CUT DEPTH	5	0.47	0.26	0.15	0.0	-0.2	-0.3	-0.4 -0.4	-0.4	-0.3	-0.2	-0.2	-0.0	30.0	0.70		0.05	0.0		0.1 ² 0.16	0.33		0.46	0.54	0.54	0.62	0.47	0.40	-0.2	-0.4	-0.8	-0.8	-0.8	-0.9 -0.9	-1.0	-1.0		 	-1.0	-1.0		-0.8 -0.8	-0.8	-0.7	-0.6	-0.5	2.0-
Television 358.13 358.13 358.27 358.27 358.27 358.27 358.27 358.27 358.27 358.27 358.27 358.27 358.27 358.27 358.27 355.66.29 356.28 366.66 366.66 366.66 366.73 355.66.23 355.28 366.73 355.66.23 356.29 366.73 355.66.23 356.673 366.73 355.66.73 356.66.73 366.67 366.68 366.68 366.73 355.28 356.63 366.73 355.68 366.73 366.73 355.68 366.67 366.73 355.68 366.73 366.73 369.69 369.69 369.66 369.69 369.69 369.67 369.68 369.68 369.68 369.68 369.68 369.68 369.69 369.68 369.68 369.68 369.68 <t< td=""><td></td><td></td><td>358.22</td><td>358.23 358.27</td><td>358.29</td><td>358.46 358.63</td><td>358.71</td><td>358.93</td><td>359.63</td><td>359.82</td><td>360.43</td><td>361.11 361.23</td><td>361.26</td><td>362.03</td><td>362.66</td><td>362.82</td><td>363.30</td><td>363.40</td><td>363.69 363.87</td><td></td><td>364.24 364.34</td><td>364.81</td><td>יר ספר</td><td>365.28 365.28</td><td>365.83</td><td>365.93</td><td>366.25</td><td>366.73</td><td>366.86 367.89</td><td>368.60</td><td>368.90</td><td>369.39 360.44</td><td>369.54</td><td>369.69</td><td>369.76</td><td>369.80</td><td>369.81</td><td>369.82</td><td>369.85 369.84</td><td>369.86</td><td>369.87</td><td>369.88</td><td>309.04 369.82</td><td>369.68</td><td>369.44 369.02</td><td>368.78</td><td>368.60 367 87</td><td>367.83</td></t<>			358.22	358.23 358.27	358.29	358.46 358.63	358.71	358.93	359.63	359.82	360.43	361.11 361.23	361.26	362.03	362.66	362.82	363.30	363.40	363.69 363.87		364.24 364.34	364.81	יר ספר	365.28 365.28	365.83	365.93	366.25	366.73	366.86 367.89	368.60	368.90	369.39 360.44	369.54	369.69	369.76	369.80	369.81	369.82	369.85 369.84	369.86	369.87	369.88	309.04 369.82	369.68	369.44 369.02	368.78	368.60 367 87	367.83
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---- EXISTING SURFACE



FOR RESOURCE CONSENT

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REV.	REVI	SION DETAIL	S			DATE
А	ORIG	INAL ISSUE				30/03/22
В	FOR	RESOURCE	CONSENT			27/09/22
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		TP CH. 3.29 RL.350.87	SAC CH 0.20 BI 350 78	340 CH. 9.29 KL.330.70	VTP CH. 14.69 RL.350.85		VTP CH 29 85 BI 351 26		- CRESI CH. 35.25 RL.351.33	VTP CH. 42.25 RL.351.21		2			VTP CH. 62.57 RL.350.50		 VIP CH. 70.07 RL.350.24 									E VIP CH. 119.62 KL.349.99 SAG CH. 121.12 RL.349.99	VTP CH. 122.62 RL.349.99					 VTP CH. 149.01 RL.350.12 	VIP CH. 153.16 RL.350.14 VID CH. 153.16 RL.350.14	T VIP CH. 157.32 KL.350.28	1	
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EXISTING GROUND	350.07	349.96	349.81	349.81	349.81 349.82	349.78	349.56	349.56	349.51	349.51	349.49	349.47	349.43	349.21	349.19	349.18	349.11	349.02	349.11	349.43	349.15	349.21	349.30	348.80	34036	349.43	349.69	349.79	349.84	349.77	349 44	349.37	349.20	349.17	349.21	349.21
+ FILL DEPTH - CUT DEPTH	06.0	0.91	0.97	0.97	0.97 1.03	1.21	1.70	1.71	1.82	1.82	1.79	1.74	1.0.1	1.38	1.34	1.32	1.18	1.18	1.08	0.71	0.96	0.89	0.79	1.24	0.63	0.56	0.29	0.20	0.19	0.30	0.68	0.76	0.97	1.11	1.16	1.18
DESIGN LEVEL	350.97	350.87	350.78	350.78	350.78 350.85	350.99	351.26	351.26	351.33	351.33	351.28	351.21	350.94	350.59	350.53	350.50	350.29	350.20	350.19	350.14	350.11	350.10	350.09	350.04	349 99	349.99	349.99	349.99	350.03	350.08	350.12	350.13	350.17	350.28	350.37	350.39
CHAINAGE	0.00	3.29	8.99	9.29	10.00	20.00	29.85	30.00	35.25	36.05	40.00	42.25	00.00	59.95	61.79	62.57	70.00	77.57	80.00	90.00	96.26	98.23	100.00	110.00	119.62	120.00	121.12	122.62	130.00	140.00	149.01	150.00	153.16	157.32	160.00	160.71
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BY: Sb

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	Client/Location: WATERFALL PARK DEVELOPMENTS LTD LOT 1 DP 540788						
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WATERFALL PARK DEVELOPMENTS LTD LOT 1 DP 540788					
PurposeDrawing Title: NORTHBROOK - ARROWTOWN BRIDGE 01 LONGSECTION					
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PLANS DWG



LEGEND

LEGAL BOUNDARY (SUBJECT PROPERTY)

- LEGAL BOUNDARY (ABUTTALS)
- MILL CREEK
- SITE EXTENT
 - CATCHMENT EXTENT (PRIMARY NETWORK)
- RAIN GARDEN
- OPEN SWALE \leftarrow
- KERB / CONCRETE CHANNEL
 - SHEET FLOW DIRECTION
 - STORMWATER PIPE / CULVERT
- MUDTANK / MANHOLE
- ------ FLOOD EXTENT 100y ARI
 - PROPOSED BUILDING
- - - FLOOD EXTENT/FREEBOARD RL

NOTES

- REFER TO CKL REPORT FOR DETAILS OF SW TREATMENT ROOF RUNOFF WILL BE PIPED DIRECTLY TO OPEN SWALES AND BE CONVEYED TO MILL CREEK,
- 3.
- ALL CATCHMENT EXTENTS SHOWN ARE INDICATIVE ONLY, AREA MAY CHANGE DURING DETAILED DESIGN.

FOR RESOURCE CONSENT

REV.	REVISION DETAILS	DATE
А	ORIGINAL ISSUE	30/03/22
В	FOR RESOURCE CONSENT	12/06/22
С	RFI RESPONSE	28/02/23

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WATERFALL PARK **DEVELOPMENTS LTD** LOT 1 DP 540788

pose/Drawing Title

liont/Loc

NORTHBROOK - ARROWTOWN STORMWATER LAYOUT

Surveyed by:		Original Size:	Scale:	
Designed by:	SB		1.500	
Drawn by:	SB	Δ3	1.500	
Checked by:	SP] /.0		
Approved by:			DO NOT SCALE	
Job Ref: Q6388 -	82 - 01	Sheet No: 401	Revision No: Date Issued: C 28/02/2023	

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LEGEND

LEGAL BOUNDARY (SUBJECT PROPERTY)

- LEGAL BOUNDARY (ABUTTALS)
- MILL CREEK
- SITE EXTENT
 - CATCHMENT EXTENT (PRIMARY NETWORK)
- RAIN GARDEN
- OPEN SWALE
- - SHEET FLOW DIRECTION
 - STORMWATER PIPE / CULVERT
- MUDTANK / MANHOLE
- ------ FLOOD EXTENT 100y ARI
 - PROPOSED BUILDING
- - FLOOD EXTENT/FREEBOARD RL

NOTES

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liont/Loc

WATERFALL PARK **DEVELOPMENTS LTD** LOT 1 DP 540788

Purpose/Drawing Title:

NORTHBROOK - ARROWTOWN STORMWATER LAYOUT

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LEGAL BOUNDARY (SUBJECT PROPERTY)

- LEGAL BOUNDARY (ABUTTALS)
- MILL CREEK
- SITE EXTENT

CATCHMENT EXTENT (PRIMARY NETWORK)

RAIN GARDEN

---- OPEN SWALE

SHEET FLOW DIRECTION

- STORMWATER PIPE / CULVERT

MUDTANK / MANHOLE

------ FLOOD EXTENT 100y ARI

PROPOSED BUILDING

FLOOD EXTENT/FREEBOARD RL

NOTES

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Client/Loca



urpose/Drawing Title:

NORTHBROOK - ARROWTOWN STORMWATER LAYOUT

Surveyed by:		Original Size:	Scale:	
Designed by:	SB		1.500	
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Approved by:			DO NOT SCALE	
Job Ref: Q6388 - 8	32 - 01	Sheet No: 404	Revision No: Date Issued: C 28/02/2023	

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С	RFI RESPONSE	28/02/23

QUEENSTOWN.
Terrace Junction,
1092 Frankton Road
PO Box 2645,
Ouconstown 0340

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